Parallel three-dimensional simulations of quasi-static elastoplastic solids

Nicholas M. Boffi & Chris Rycroft July 16, 2019

Harvard University, Department of Applied Mathematics. CSGF Program Review 2019.

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 - Stronger than steel, with high strength to elasticity ratio.
 - Can be processed and molded like a plastic.
- Applications limited by catastrophic failure mechanism: shear banding.





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- · Shear band: rapid (ms) narrow (10 nm) localization of plastic deformation due to a strain-softening instability.
- Physics: Any theory of amorphous plasticity must be able to predict structure and formation of shear bands.
- · Applications: Until shear bands are understood and controlled, BMGs cannot be used in practice.



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- STZs: localized regions likely to undergo small-scale plastic rearrangements.
- Randomly distributed with Boltzmann density in an effective disorder temperature χ .
- χ is measured in Kelvin, $\chi \propto \frac{\partial (\text{Config. Energy})}{\partial (\text{Config. Entropy})}$, but distinct from usual kinetic/vibrational temperature T.





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Linear Elasticity $\begin{array}{l} \text{Stiffness} \\ = \ \widehat{\mathbf{C}} \ : \underbrace{\mathbf{D}^{el}}_{\text{Elastic Part}} \end{array}$ $\frac{\mathcal{D}\sigma}{\underbrace{\mathcal{D}t}} \stackrel{\text{Sti}}{=}$ Truesdell Rate









$$\underbrace{\mathbf{D}^{pl}}_{\text{Plastic rate}} = \underbrace{D^{pl}f(\sigma)}_{\propto \text{ deviatoric}}$$



$m \times a$

Shear Transformation Zone Theory

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 $D^{
m pl} \propto (
m Density of STZs) \times (
m Arrhenius barrier crossing)$ $\times (
m Rates for forward and reverse transitions) \times \left(1 - \frac{s_y}{\pi}\right)$

 $\times \begin{cases} 1 & \text{ if local stress above yield stress} \\ 0 & \text{ else} \end{cases}$

Hypo-elastoplastic long-time limit Incompressible limit of Navier-Stokes

Hypo-elastoplastic long-time limit

$$\frac{\mathcal{D}\sigma}{\mathcal{D}t} = \mathbf{C} : \left(\mathbf{D} - \mathbf{D}^{\mathsf{pl}}\right)$$

hypo-elastoplastic equation

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From Navier-Stokes to hypo-elastoplasticity

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Hypo-elastoplastic long-time limitIncompressible limit of Navier-Stokes $\underbrace{\frac{D\sigma}{Dt} = \mathbf{C} : (\mathbf{D} - \mathbf{D}^{pl})}_{\text{hypo-elastoplastic equation}}$ $\underbrace{\frac{\rho \, d\mathbf{v}}{dt} = -\nabla p + \nabla \cdot \mathbf{T}}_{\text{Navier-Stokes equation}}$ $\underbrace{\frac{\nabla \cdot \sigma \approx 0}{\text{Quasi-static constraint}}}$ $\underbrace{\frac{\nabla \cdot \mathbf{v} \approx 0}{\text{Incompressibility constraint}}$





- · Any algorithm for Navier-Stokes should work for hypo-elastoplasticity.
- This analogy is independent of the plasticity model.

Hypo-elastoplastic equation

• Continuous-time:

$$\frac{\mathcal{D}\sigma}{\mathcal{D}t} = \mathbf{C} : \left(\mathbf{D} - \mathbf{D}^{\mathsf{pl}}\right)$$

• Semi-implicit Euler discretization:

$$\frac{\sigma^{n+1} - \sigma^n}{\Delta t} = \left(\frac{D\sigma}{Dt}\right)^n - \left(\mathbf{C}:\mathbf{D}^{\mathrm{pl}}\right)^n + \left(\mathbf{C}:\mathbf{D}\right)^{n+1}$$

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Advection step

· Just drop the $\mathbf{C}:\mathbf{D}$ term!

$$\frac{\sigma^*-\sigma^n}{\Delta t} = \left(\frac{D\sigma}{Dt}\right)^n - \left(\mathbf{C}:\mathbf{D}^{\mathrm{pl}}\right)^n$$

- Parallelized using domain decomposition and MPI (along with χ update).
- Solved on a staggered grid with σ and χ at cell centers and ${\bf u}$ at cell corners.

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Linear system for the velocity

• Take divergence of the projection step:

$$\nabla \cdot \sigma^* = -\Delta t \nabla \cdot (\mathbf{C} : \mathbf{D}^{n+1})$$

- Solved using a custom C++ implementation of the geometric multigrid method.
- Implementation is parallelized using MPI and interfaces with the advection step.
- · Optimal MPI decomposition computed at each level.
- C++ templates to solve for an arbitrary datatype at each point in space in this case, a 3-vector.

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Continuum-Scale

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Transformed domain

Physical domain

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- Define the transformed velocity and stress:

 $\begin{aligned} \mathbf{V} &= \mathbf{T}^{-1} \left(\mathbf{v} - \frac{\partial \mathbf{T}}{\partial t} \mathbf{X} \right) \\ \boldsymbol{\Sigma} &= \mathbf{T}^{-1} \boldsymbol{\sigma} \mathbf{T}^{-T} \end{aligned}$



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$$\begin{split} \frac{\partial \boldsymbol{\Sigma}}{\partial t} &= -\left(\mathbf{V}\cdot\nabla_{\mathbf{X}}\right)\boldsymbol{\Sigma} - \mathrm{tr}(\mathbf{L})\boldsymbol{\Sigma} + \boldsymbol{\Sigma}\left(\mathbf{T}^{\mathsf{T}}\mathbf{L}^{\mathsf{T}}\mathbf{T}^{-\mathsf{T}}\right) + \left(\mathbf{T}^{-1}\mathbf{L}\mathbf{T}\right)\boldsymbol{\Sigma} \\ &+ \mathbf{T}^{-1}\left(\mathbf{C}:\left(\mathbf{D}-\mathbf{D}^{\mathsf{pl}}\right) - \frac{\partial\mathbf{T}}{\partial t}\boldsymbol{\Sigma}\mathbf{T}^{\mathsf{T}} - \mathbf{T}\boldsymbol{\Sigma}\frac{\partial\mathbf{T}^{\mathsf{T}}}{\partial t}\right)\mathbf{T}^{-\mathsf{T}}. \\ \frac{\partial\mathbf{V}}{\partial t} &= -\left(\mathbf{V}\cdot\nabla_{\mathbf{X}}\right)\mathbf{V} + \frac{\partial\mathbf{T}^{-1}}{\partial t}\mathbf{T}\mathbf{V} + \mathbf{T}^{-1}\left(\mathbf{T}^{-\mathsf{T}}\nabla_{\mathbf{X}}\cdot\left(\mathbf{T}\boldsymbol{\Sigma}\mathbf{T}^{\mathsf{T}}\right) - \frac{\partial^{2}\mathbf{T}}{\partial t^{2}}\mathbf{X} - \frac{\partial\mathbf{T}}{\partial t}\mathbf{V}\right) \end{split}$$

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- + 512 \times 512 \times 256 grid.
- $\cdot \, \approx 67,000,000$ grid points in the bulk.
- Linear system matrix contains $\approx 67,000,000^2$ elements.

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Simple Shear	Pure Shear
$\mathbf{T}(t) = \begin{pmatrix} 1 & 0 & u_b t \\ 0 & 1 & 0 \\ 0 & 0 & 1 \end{pmatrix}$	$\mathbf{T}(t) = \begin{pmatrix} e^{\zeta t} & 0 & 0\\ 0 & 1 & 0\\ 0 & 0 & e^{-\zeta t} \end{pmatrix}$

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- $\cdot \, \approx 4$ day simulation time with 32 threads.

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Conclusions, Future Directions, and Acknowledgments

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