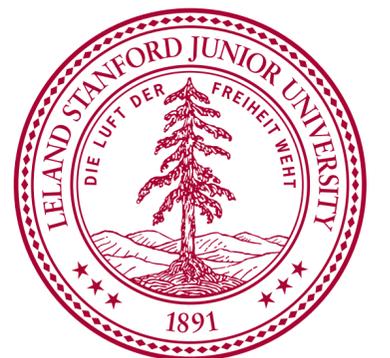


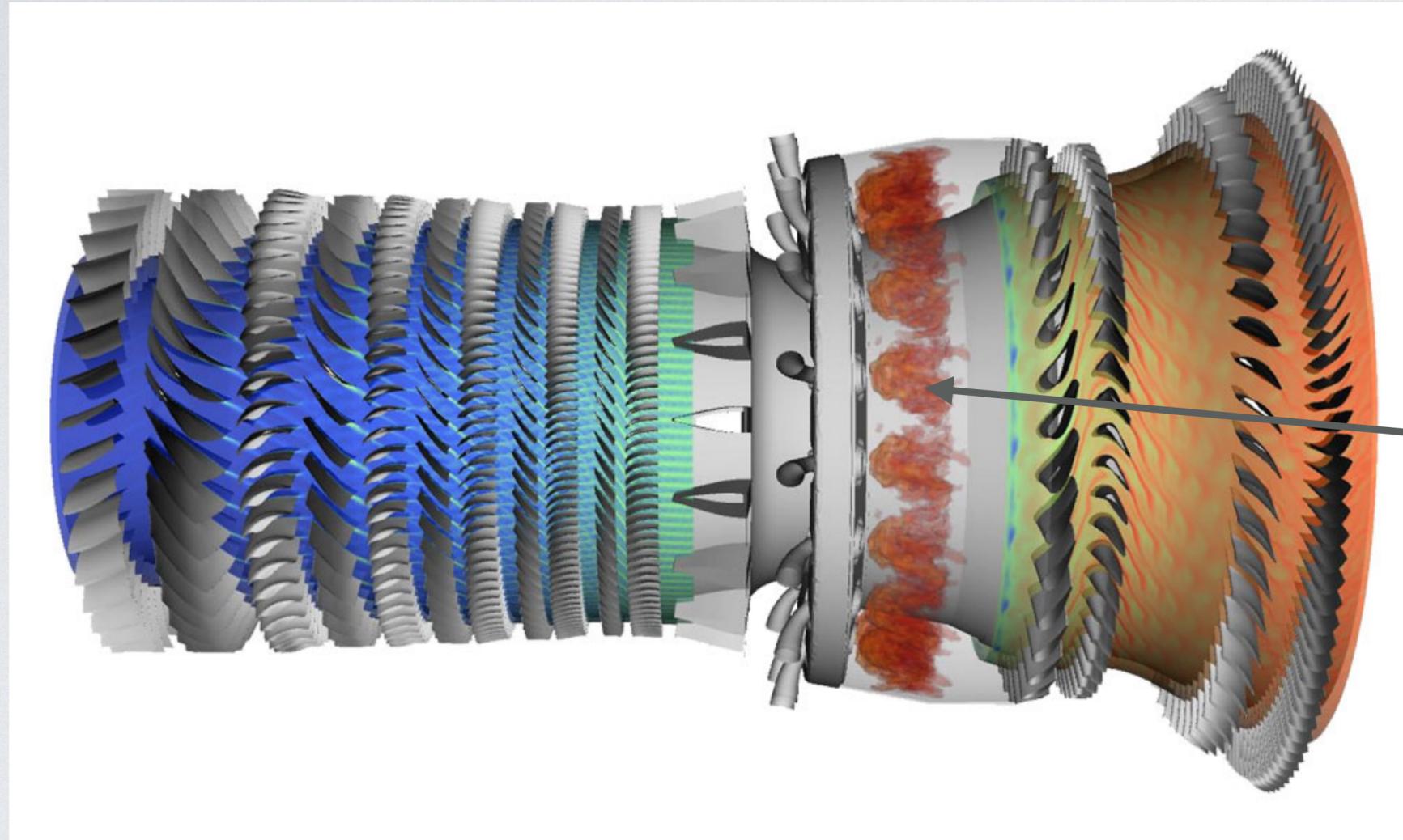
# GEOMETRIC VOLUME OF FLUID METHOD

## SIMULATION OF TWO-PHASE FLOW ON UNSTRUCTURED MESHES

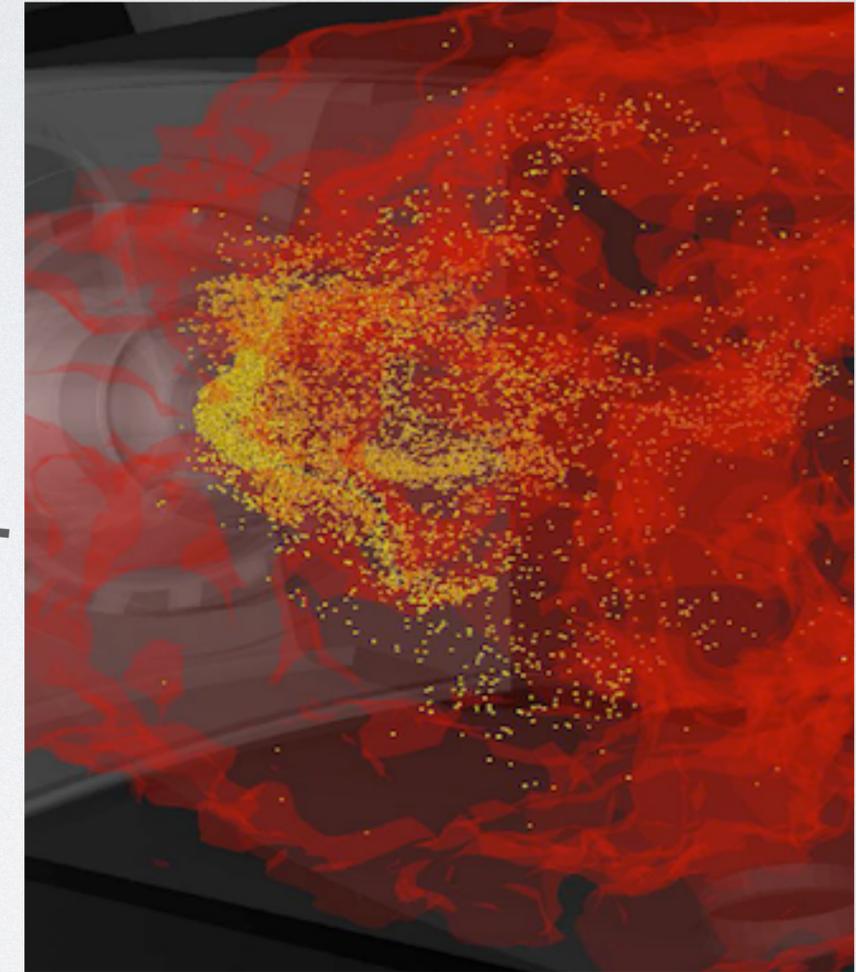
C. B. Ivey, P. Moin  
Center for Turbulence Research, Stanford University



# MOTIVATION



Pratt & Whitney 6000 turbofan engine  
Stanford ASC program



zoom of combustor sector with spray  
Cascade Technologies, Inc.

# VOLUME OF FLUID (VOF) METHOD

$$\nabla \cdot \vec{u} = 0$$

$$\frac{df}{dt} + \nabla \cdot (f\vec{u}) = 0$$

$$\frac{d(\rho\vec{u})}{dt} + \nabla \cdot (\rho\vec{u}) = -\nabla P + \nabla \cdot (\mu(\nabla\vec{u} + \nabla\vec{u}^T)) - \sigma\kappa\hat{n}\delta_S$$

$$\{\rho, \mu\} = f\{\rho_1, \mu_1\} + (1-f)\{\rho_2, \mu_2\}$$

$$\kappa = \nabla \cdot \hat{n}$$

- advection of the marker function must be conservative and bounded
- estimates of the normal and curvature must come from the marker function field

# HEIGHT FUNCTIONS

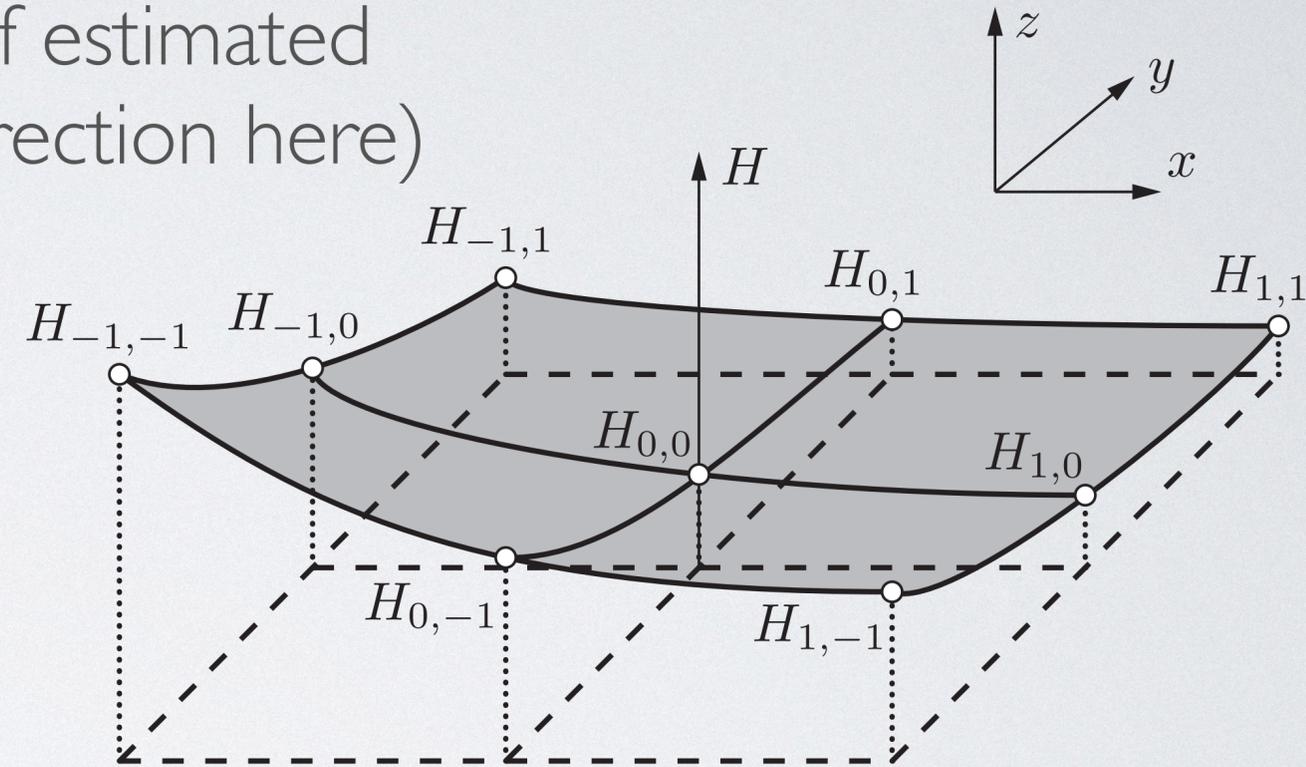
height function in direction of  
max component of estimated  
surface normal (z direction here)

$$F = \int_{\Omega} f dV$$

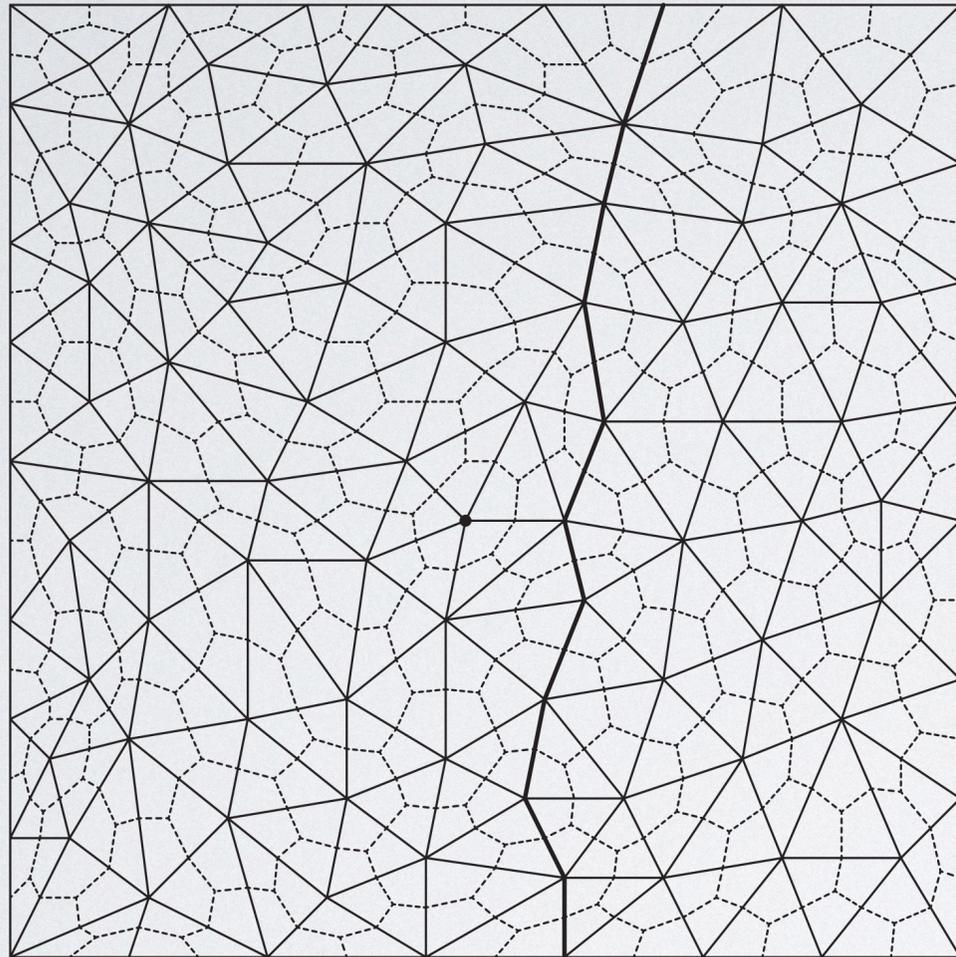
$$H_{r,s} \approx \sum_{t=-t_{down}}^{t_{up}} F_{i+r,j+s,k+t}^* \Delta z$$

$$\hat{n} = - \frac{\langle H_x \ H_y \ - \text{sign}(n_z) \rangle^T}{\sqrt{1 + H_x^2 + H_y^2}}$$

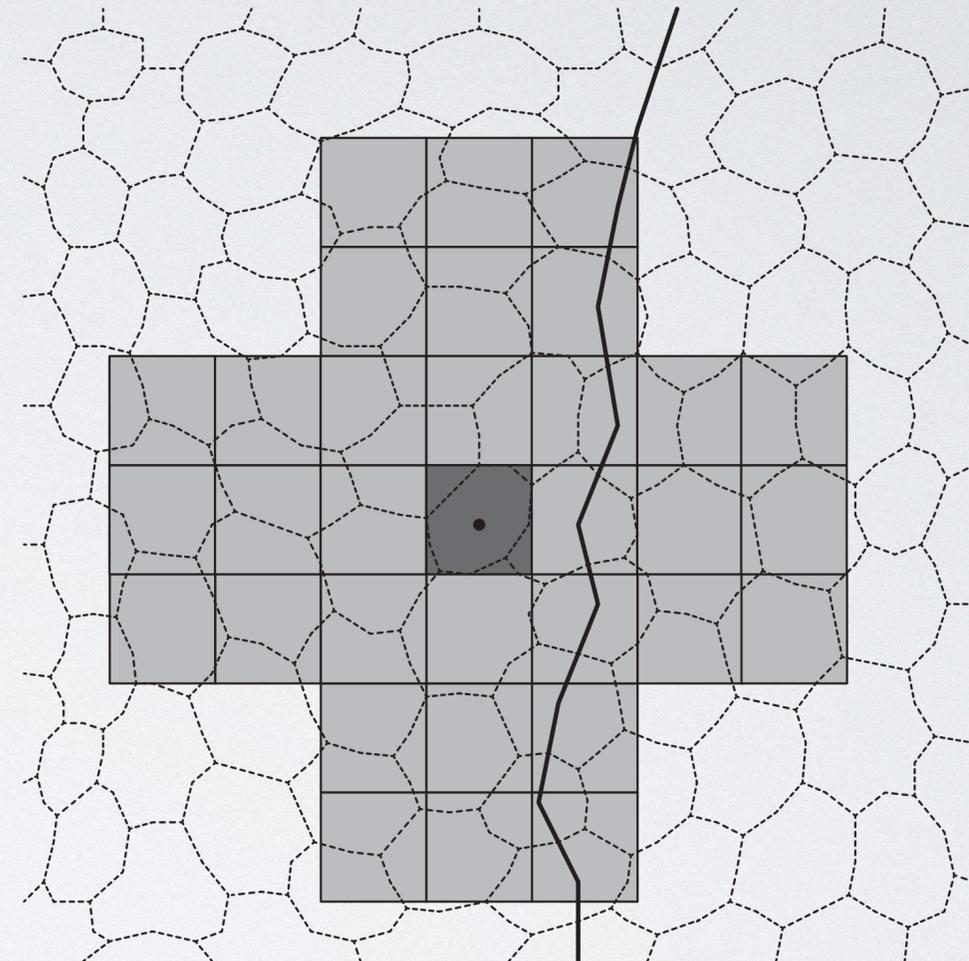
$$\kappa = - \frac{H_{xx} (1 + H_y^2) + H_{yy} (1 + H_x^2) - 2H_{xy} H_x H_y}{(1 + H_x^2 + H_y^2)^{3/2}}$$



# EMBEDDED HEIGHT FUNCTIONS (EHF)

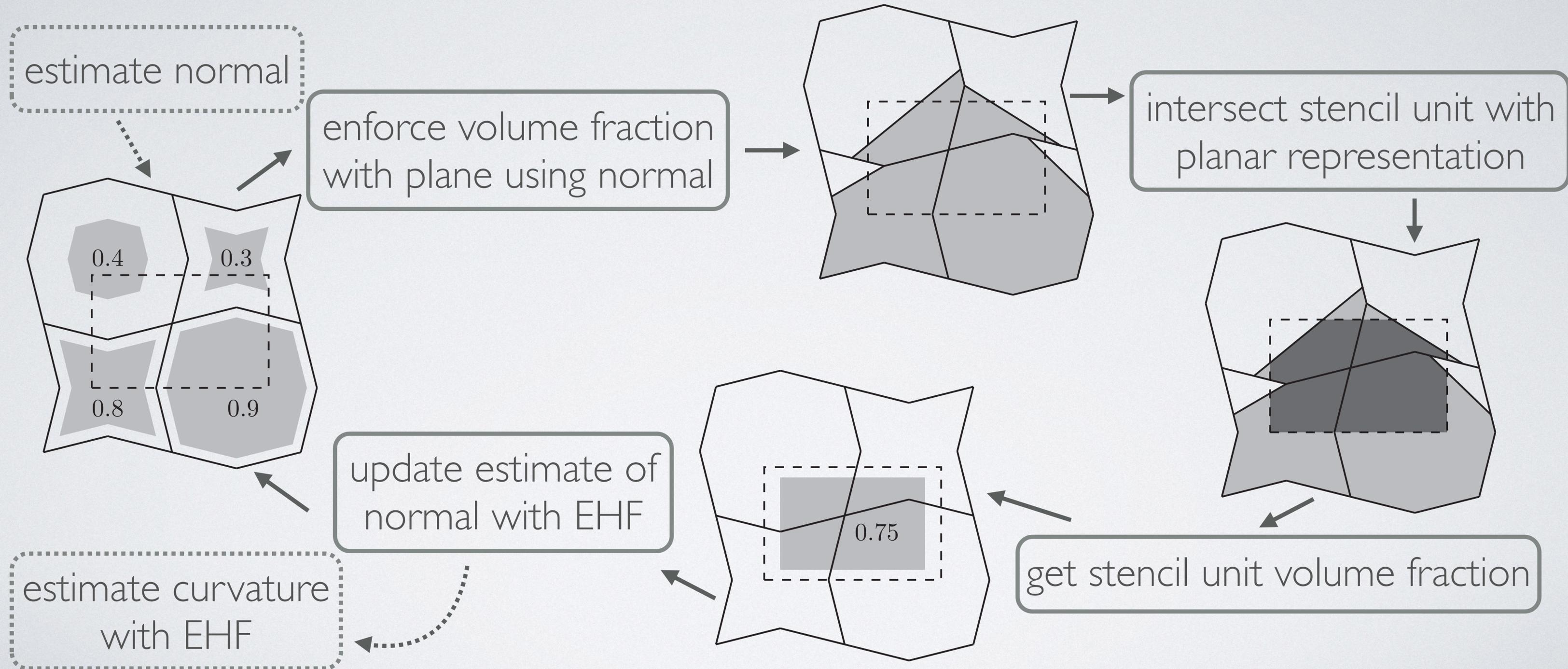


primal (solid line) and median-dual (hashed line) meshes with partitioning (thick line)



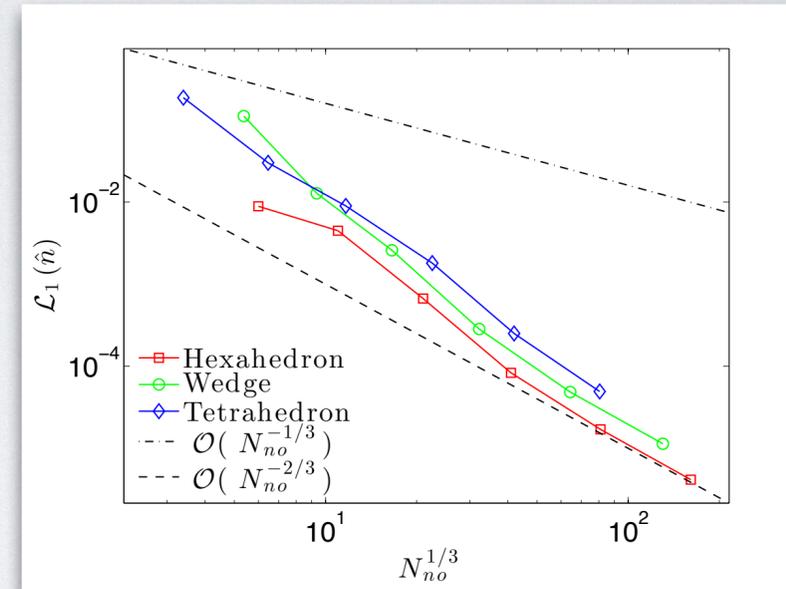
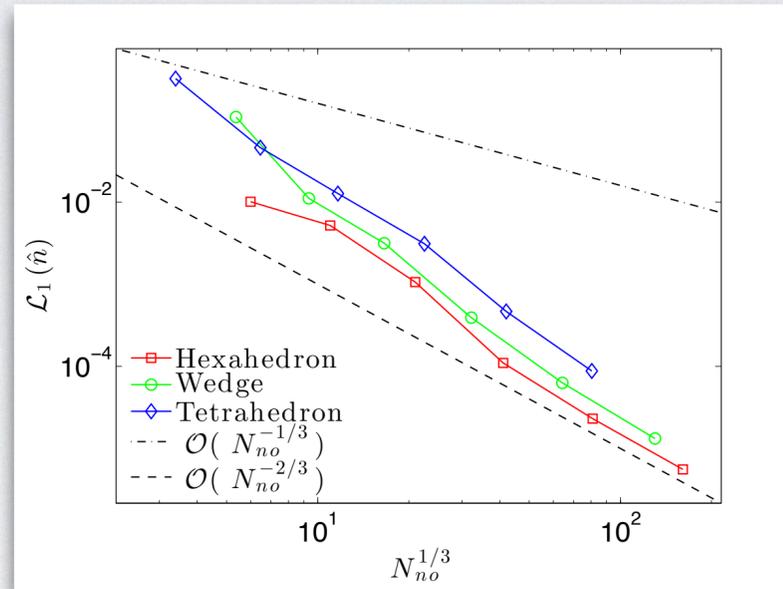
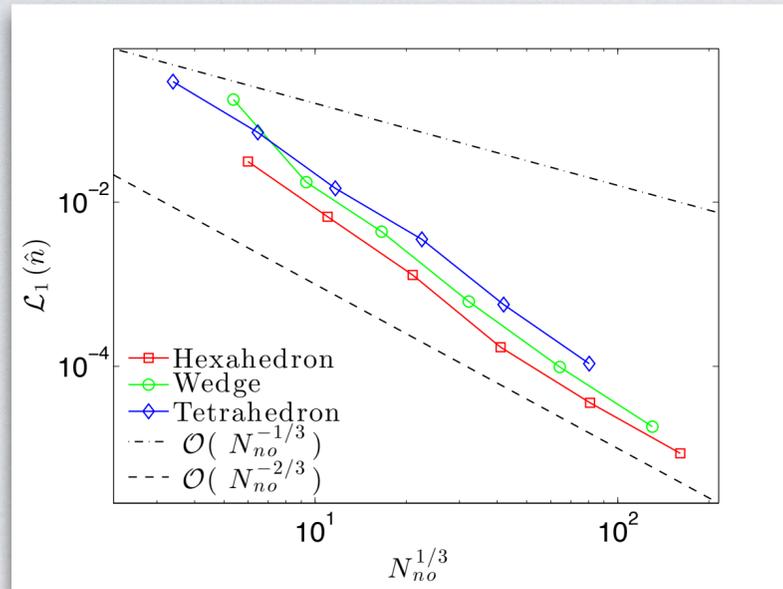
embedded cartesian stencil (light gray region) for bounding box (dark gray region) of median-dual mesh element

# PROJECTION TO EHF STENCIL

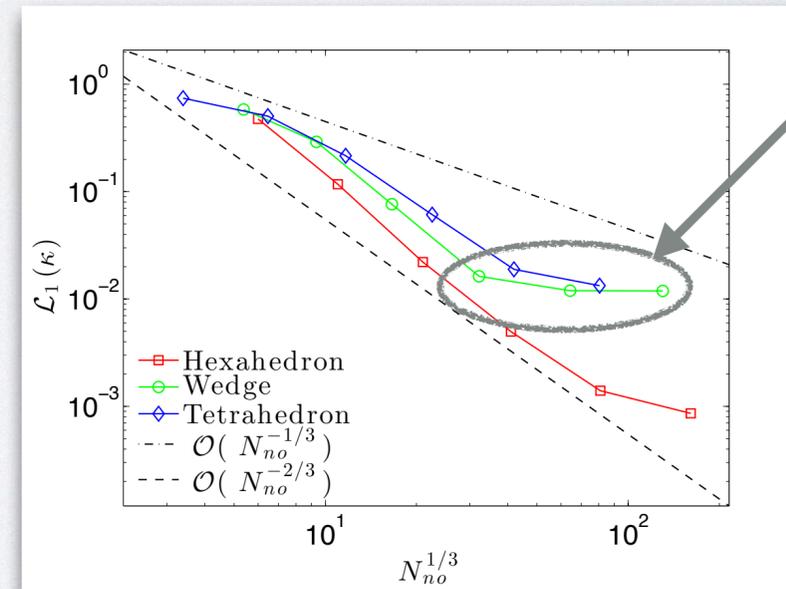
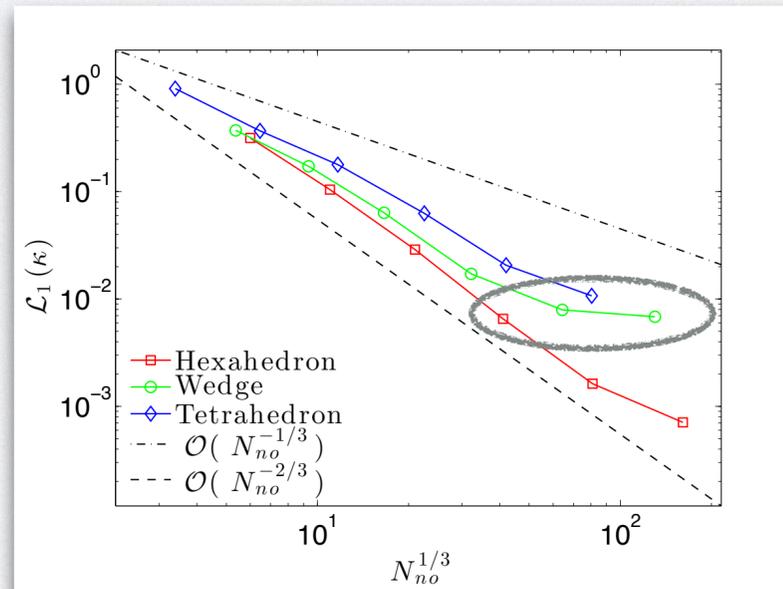
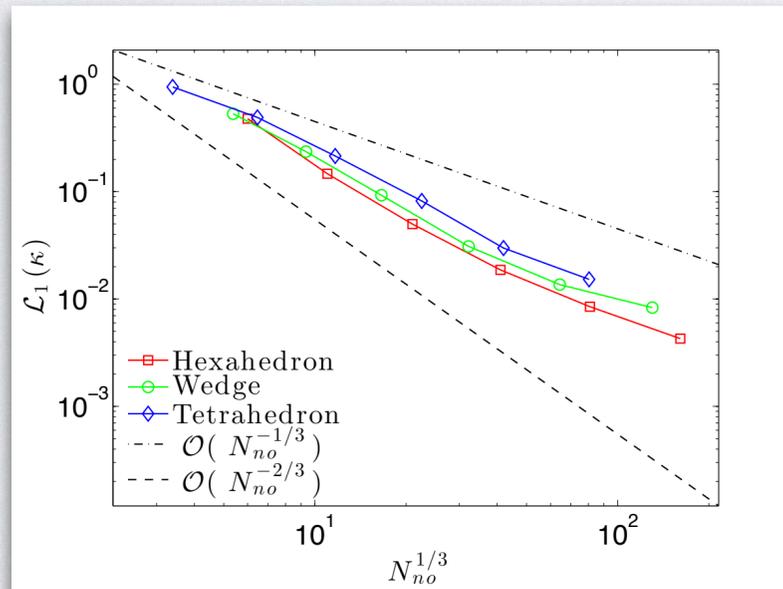


# NORMAL AND CURVATURE TESTS

normal



curvature



interpolation errors are amplified by differentiation

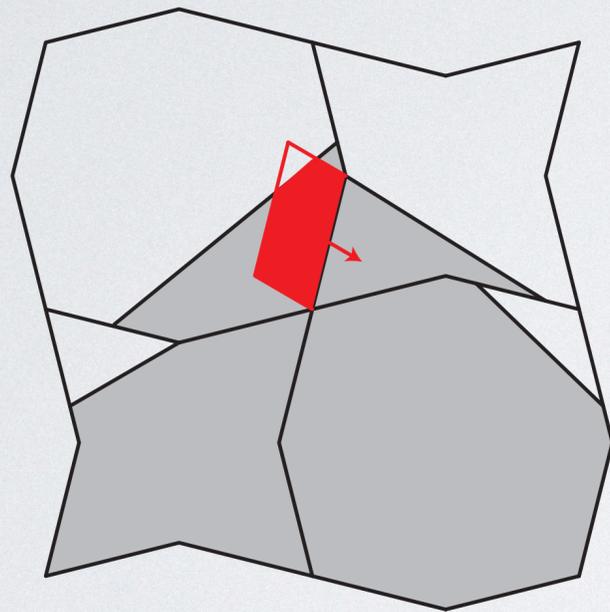
ellipsoid

sphere

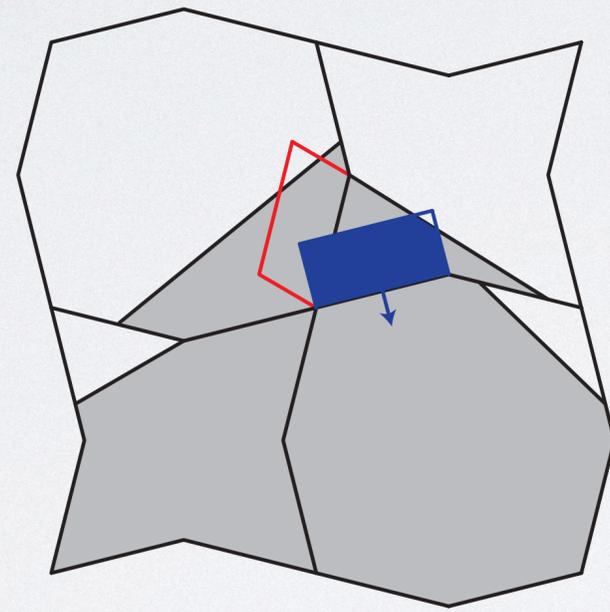
cylinder

# FLUX POLYHEDRA

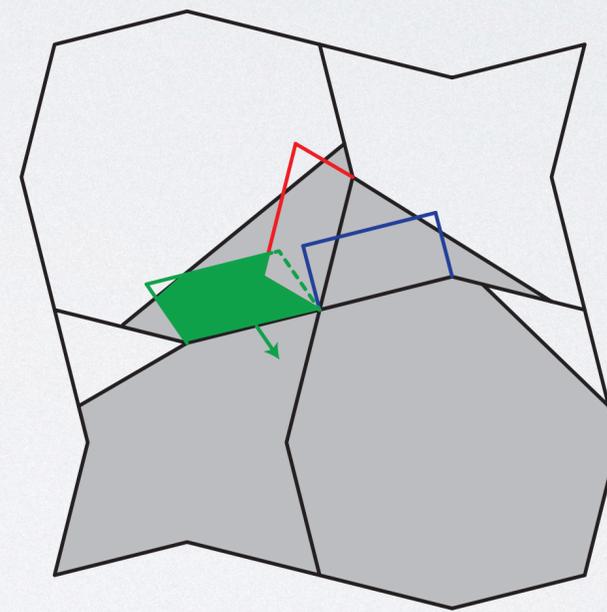
- conservation and boundedness guaranteed by preventing overlap of flux polyhedra
- accuracy depends on flux polyhedron approximation of stream tube



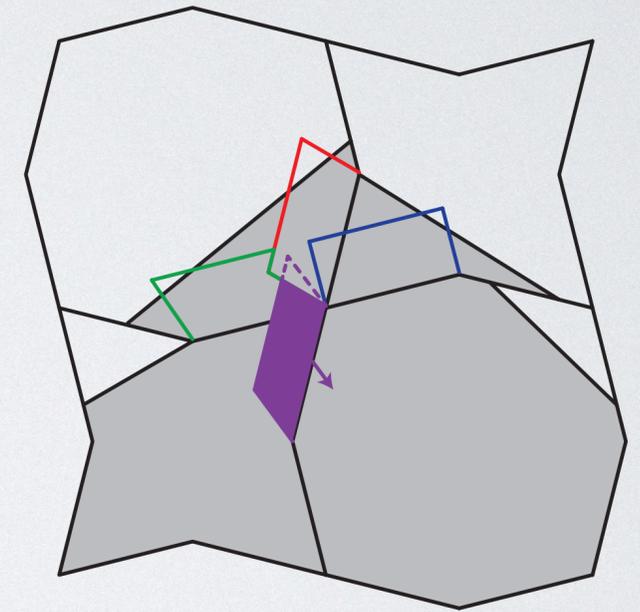
form flux polyhedron  
extruding face opposite  
velocity direction to match  
flux volume



flux polyhedron  
region is available  
to neighbor



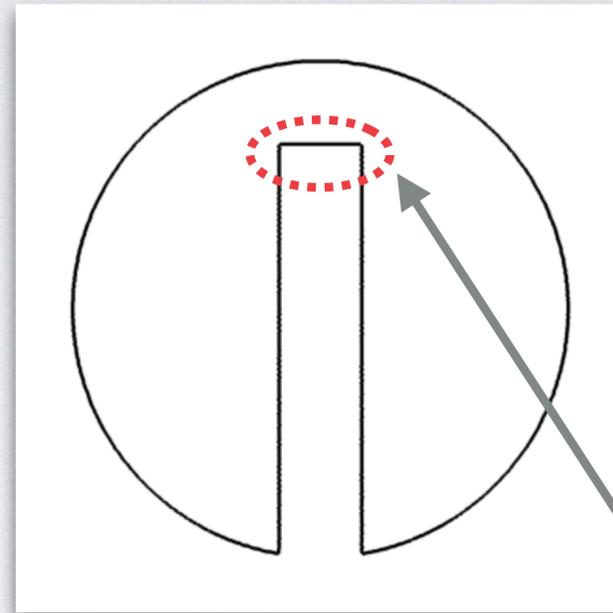
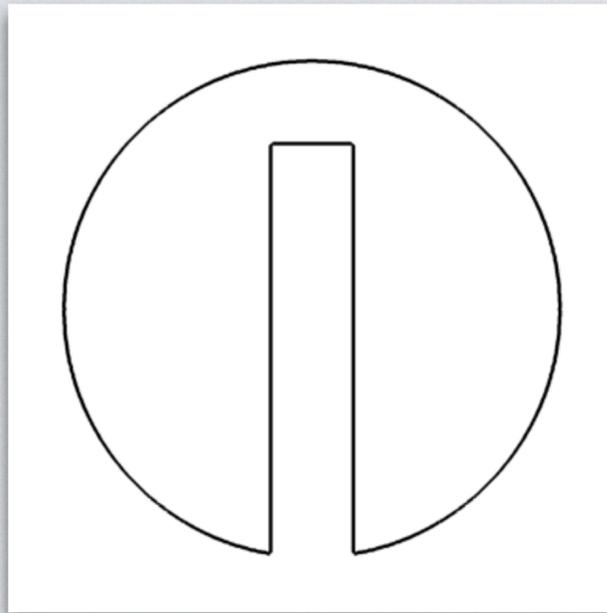
flux polyhedron  
region is unavailable  
to node



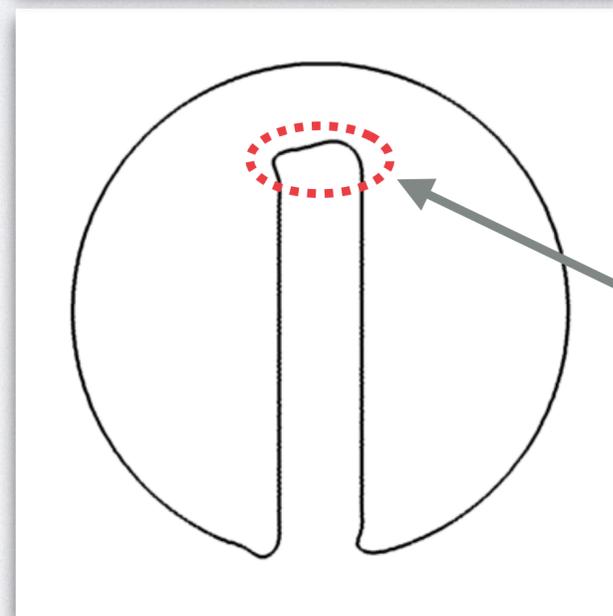
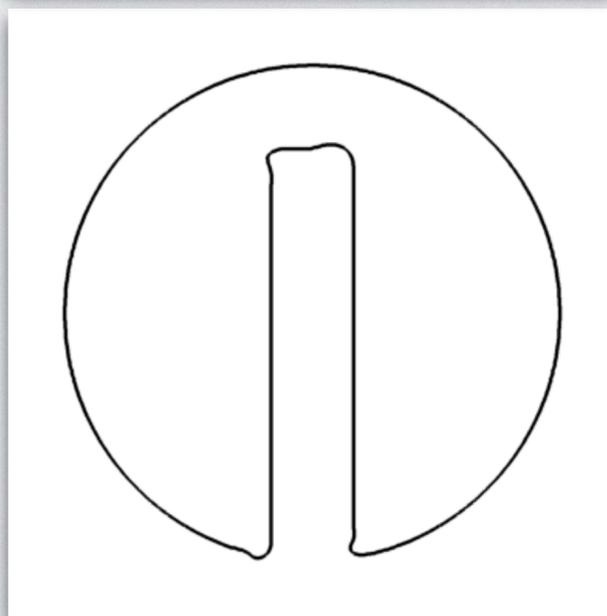
regions carry over  
into subsequent  
flux calculations

# ROTATION OF A SLOTTED DISK

0



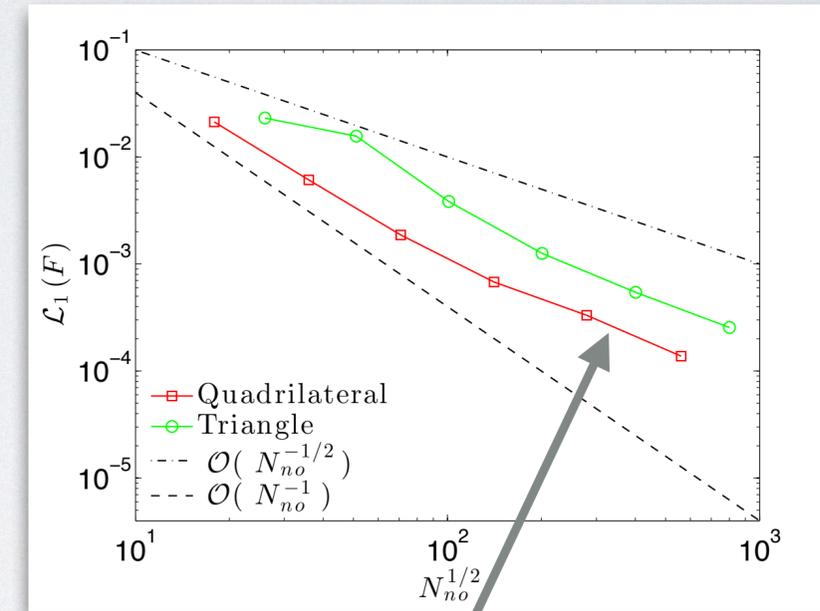
T



quadrilateral

triangle

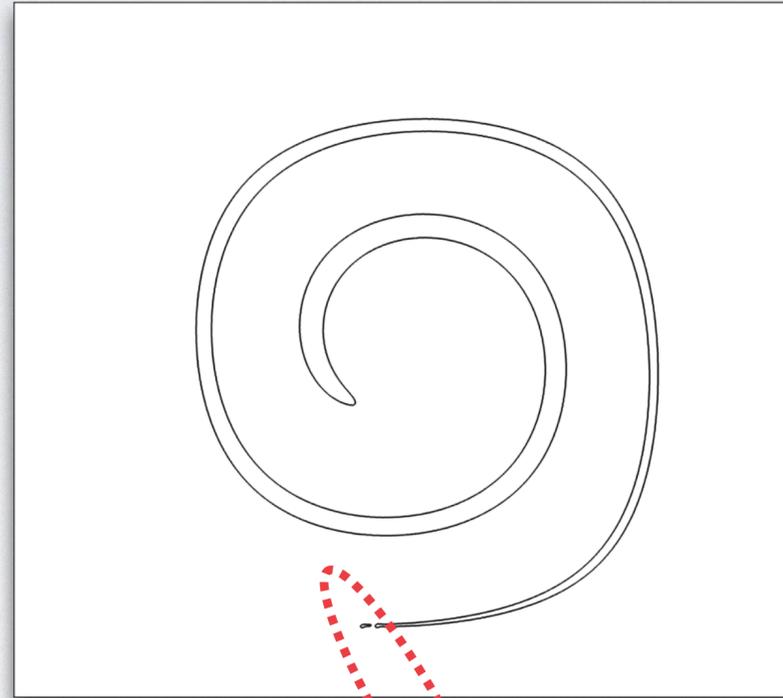
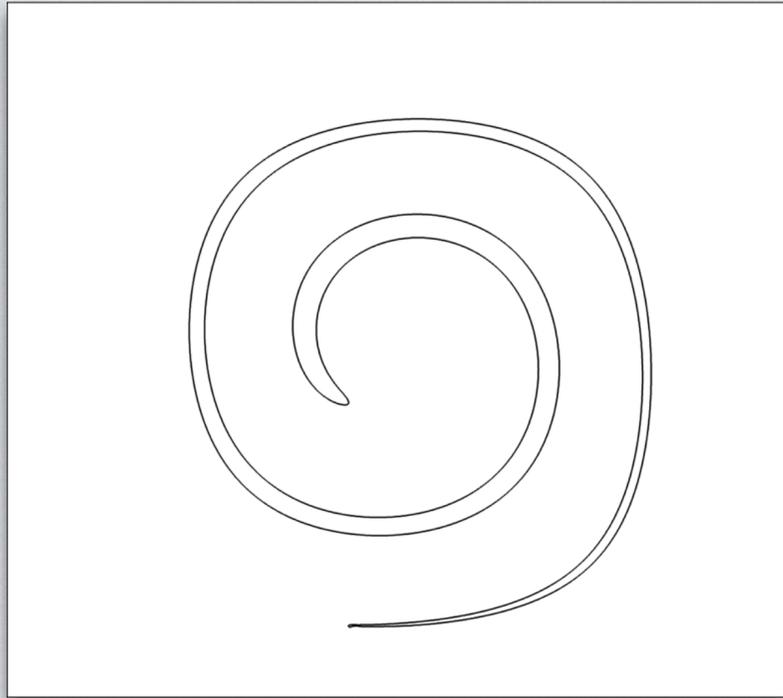
shape error



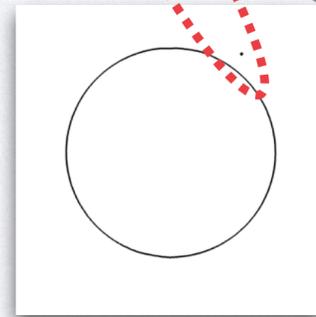
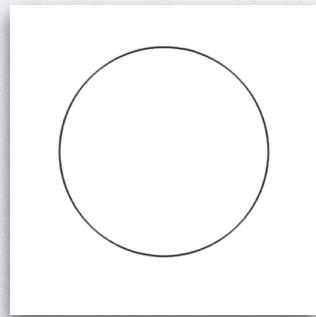
degradation in accuracy comes from sharp corners

# 2D DEFORMATION OF A CIRCLE

T/2



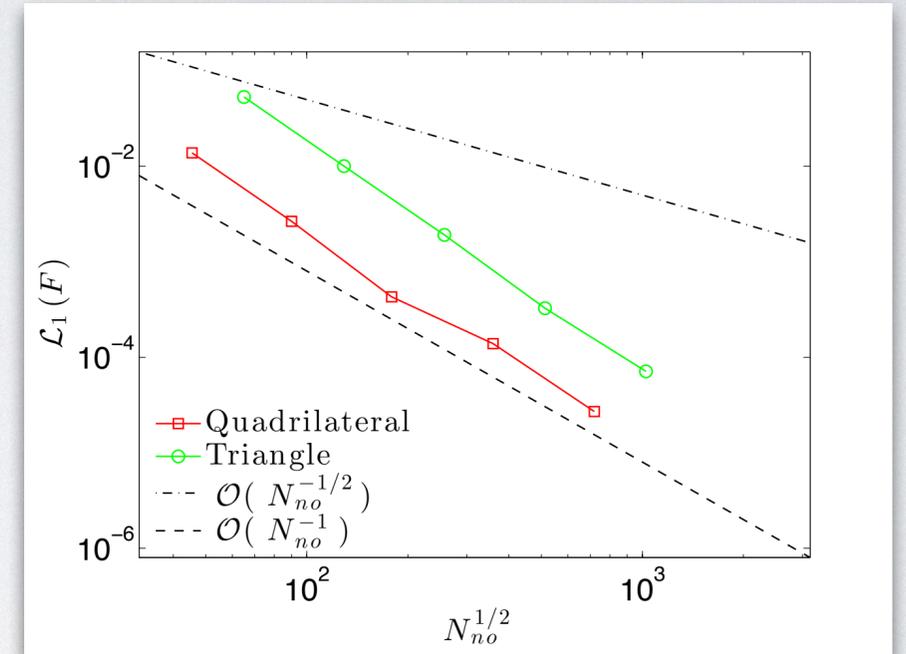
T



quadrilateral

triangle

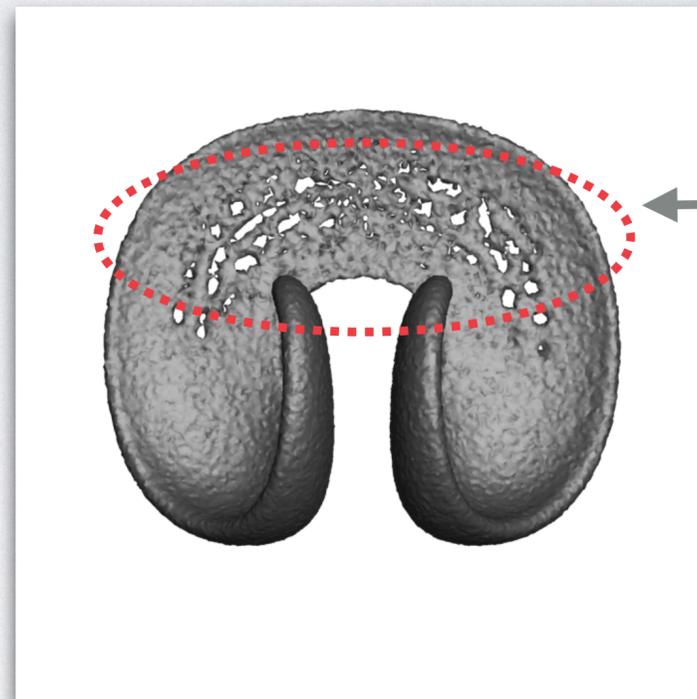
shape error



under-resolved features  
artificially breakup, leading to  
detached volume

# 3D DEFORMATION OF A SPHERE

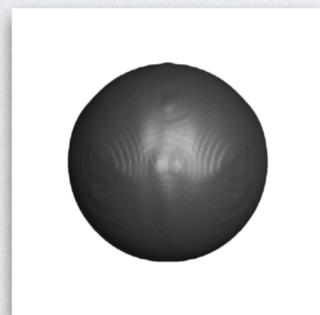
T/2



difficult to resolve thin features on tetrahedron primal mesh

shape error

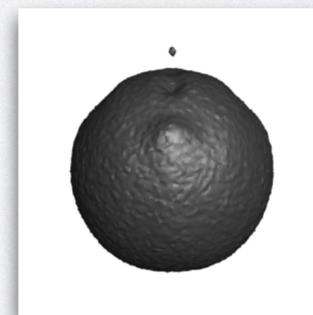
T



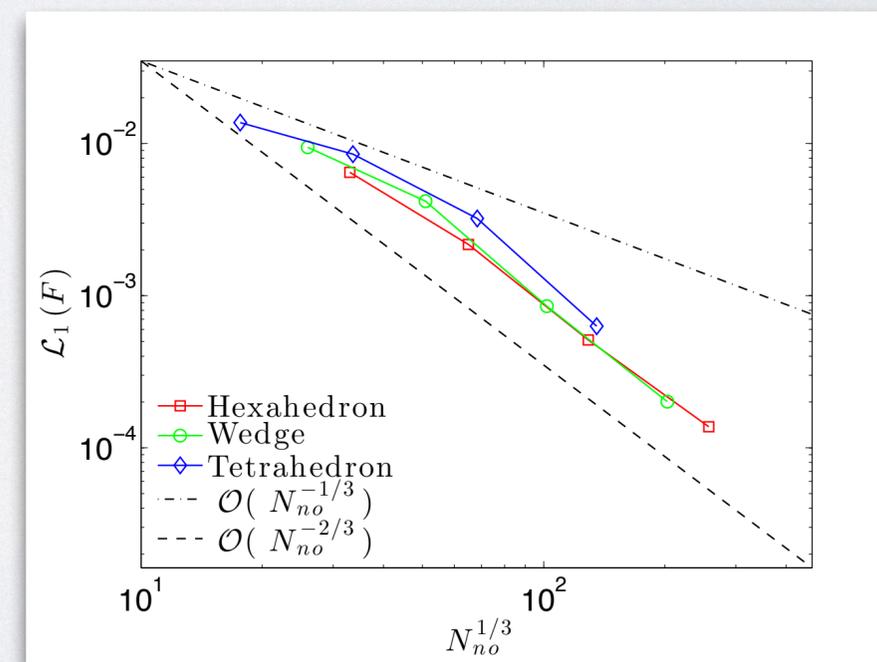
hexahedron



wedge



tetrahedron

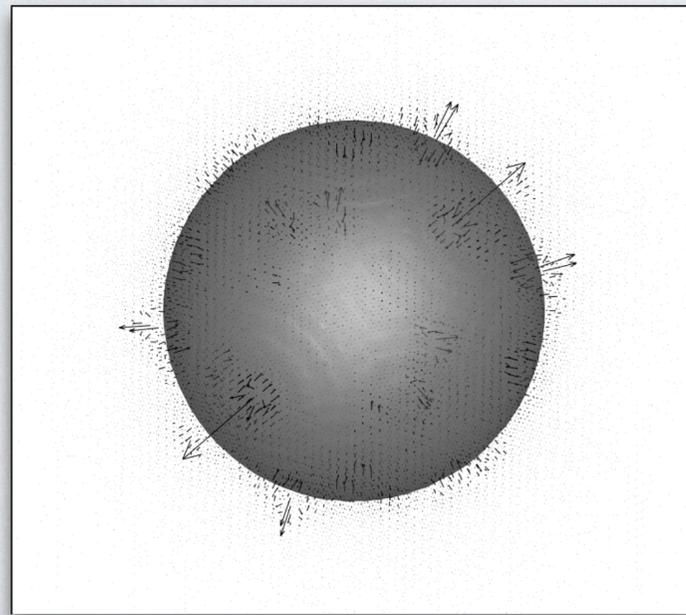


# TWO-PHASE SOLVER OUTLINE

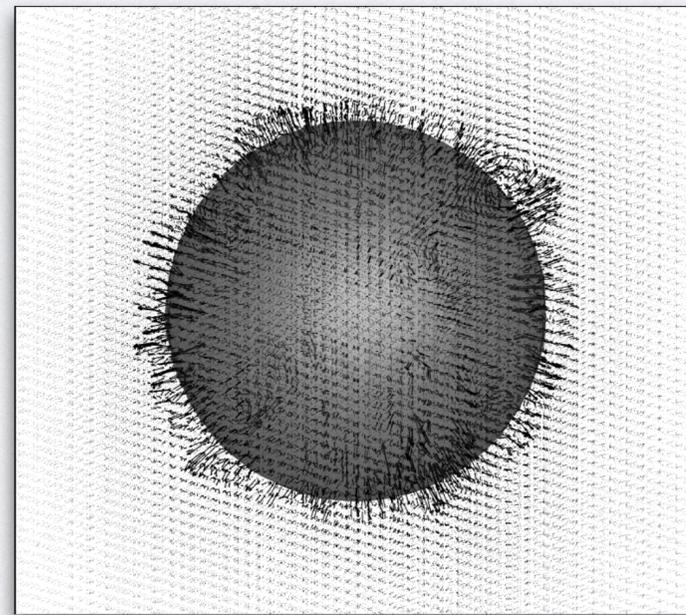
- Consistent mass (volume fraction) and momentum advection using extrapolated advection velocity
- Pressure gradient and surface tension discretely balance (so-called balanced-force method)
- Fractionally-stepped with mid-pointed pressure and surface tension
- Finite-element discretization of viscous terms with Crank-Nicholson splitting

# INVISCID STATIC DROP

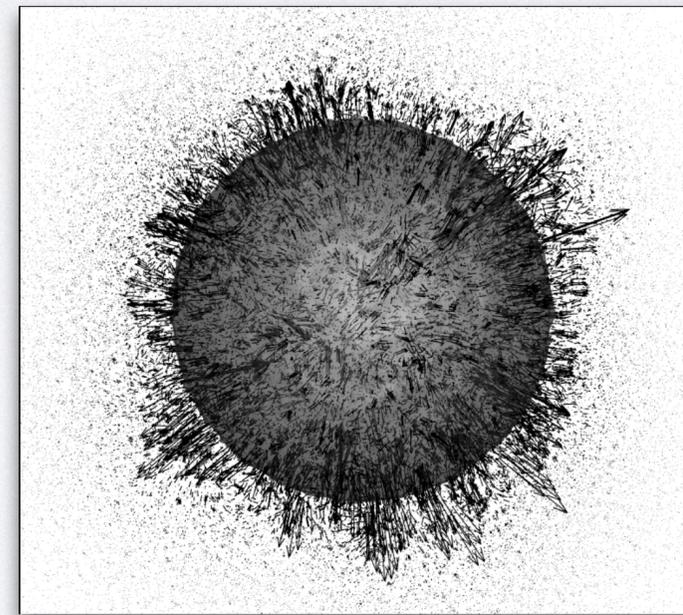
- Place a dense sphere in a static gas with a large surface tension coefficient
- Spurious currents generated only by errors in curvature



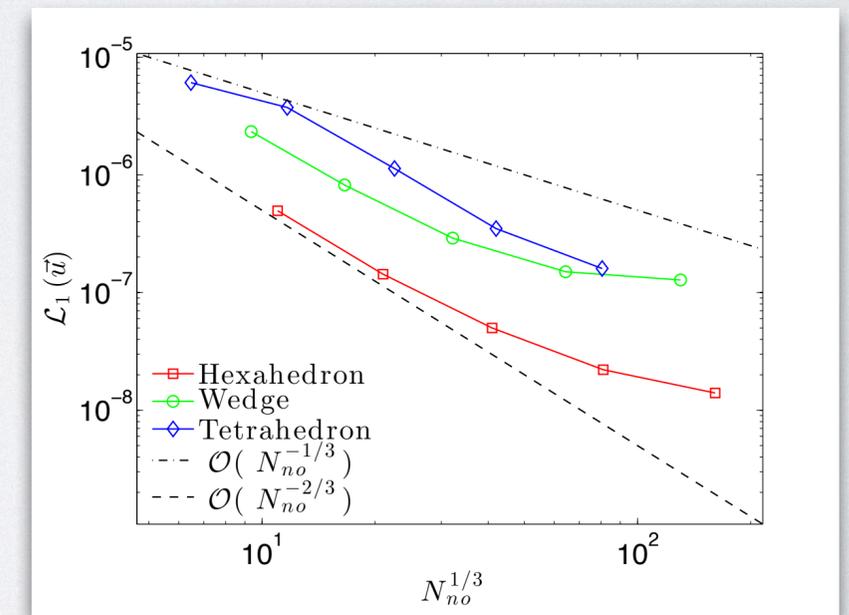
hexahedron



wedge

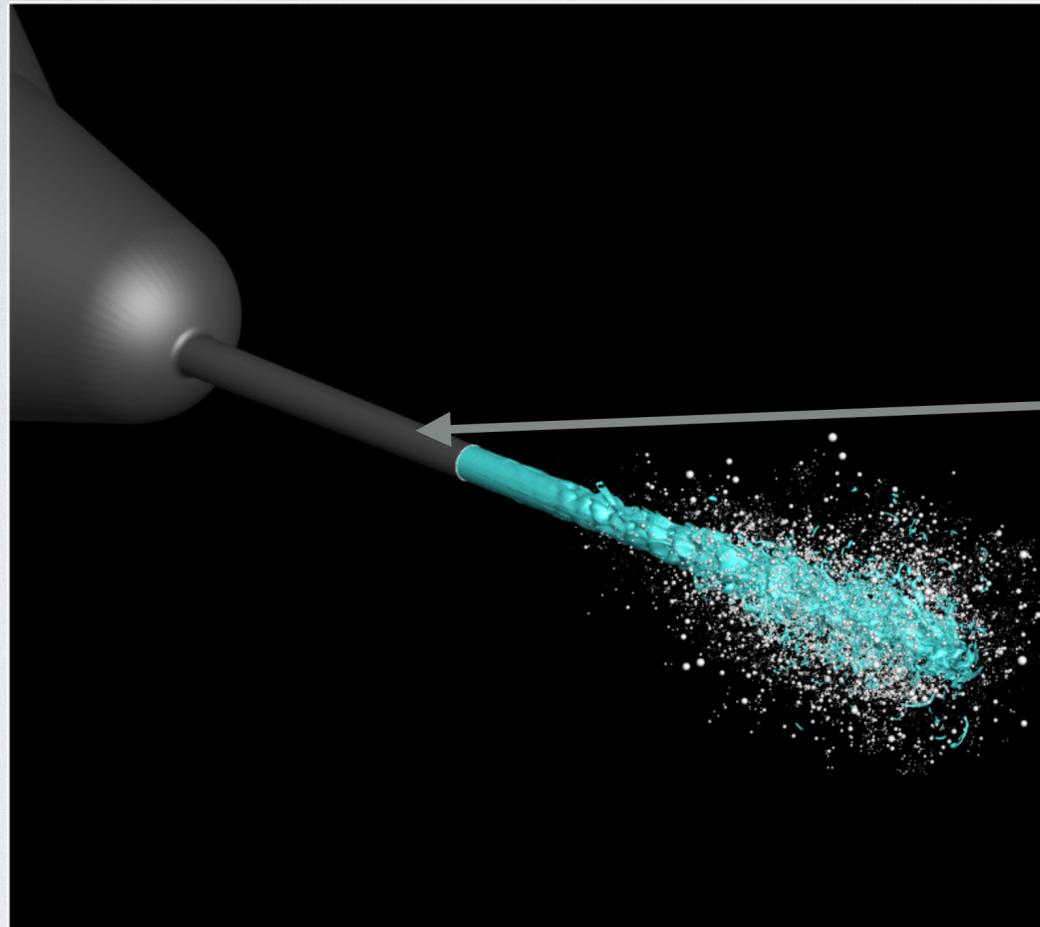


tetrahedron

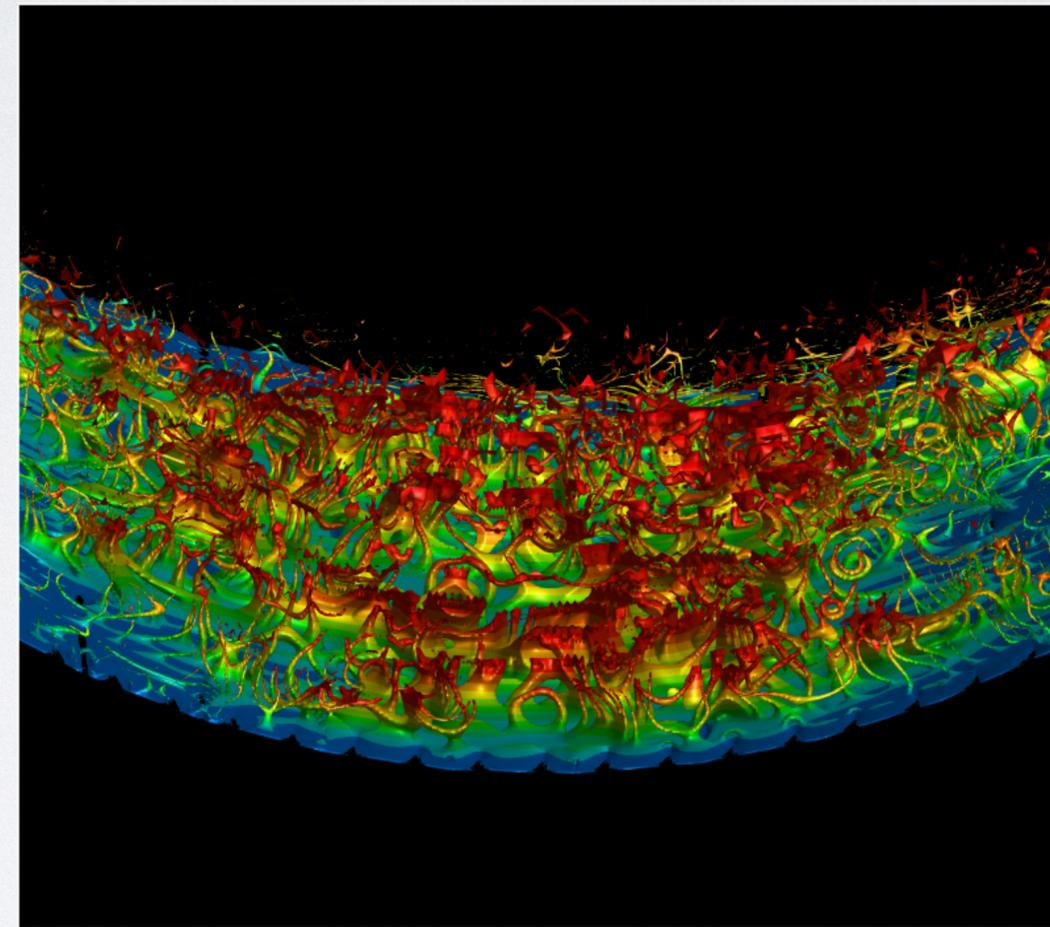


velocity error

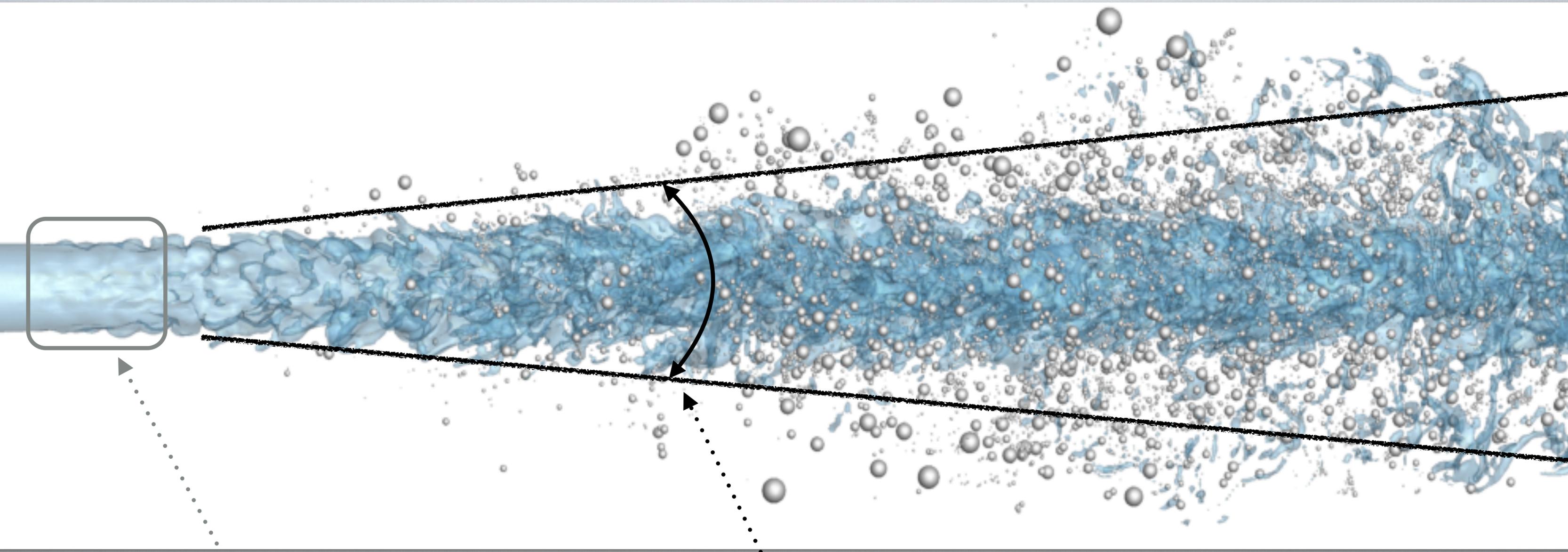
# PRIMARY ATOMIZATION OF DIESEL SPRAY FROM COMMON RAIL FUEL INJECTOR



nozzle geometry generated  
using x-ray tomography



zoom on bottom wall of nozzle  
showing turbulent structures

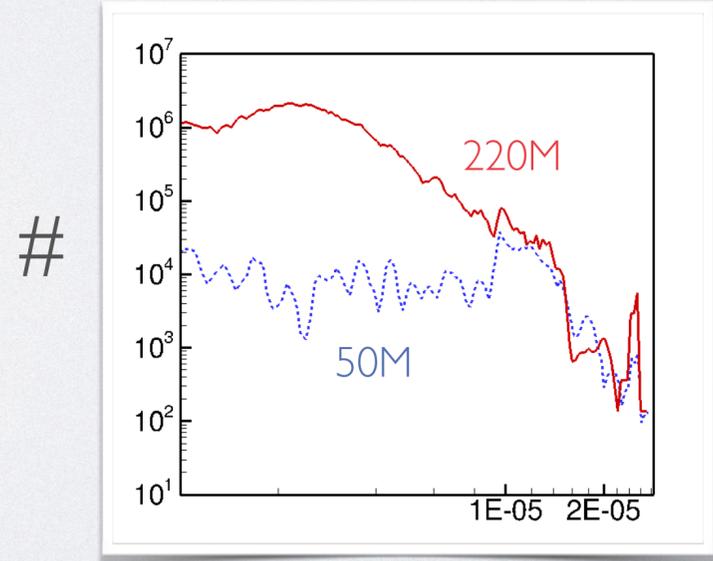


Surface perturbations  
are NOT simple  
Fourier modes

$$\theta_{simulation} = 5.1125^\circ$$

$$\theta_{theory} = 5.8325^\circ$$

$$\theta_{experiment} \approx 4^\circ$$



diameter

# CONCLUDING REMARKS

- Solving two-phase flows with large density ratios is difficult
- Solving them on unstructured node-centered meshes makes matters worse
- Leveraged a user-developed non-convex polyhedral library to develop:
  - a discretely conservative and bounded advection operator
  - a means to extract accurate and convergent normals and curvatures

# ACKNOWLEDGEMENTS

- Center for Turbulence Research, Stanford University
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- Stanford Graduate Fellowship
- ALCC compute allocation